FINAL .

SYSTEM DESCRIPTION (Index No. 28A)

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REACTOR BUILDING EMERGENCY SPRAY SYSTEM (B&R Dwg. No. 2034, Rev. 16)

JERSEY CENTRAL POWER & LIGHT COMPANY THREE MILE ISLAND NUCLEAR STATION UNIT NO. 2

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REACTOR BUILDING EMERGENCY SPRAY SYSTEM

1.0 INTRODUCTION

1.1 System Functions

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The reactor building emergency spray system serves an engineered safety features function, along with the building emergency cooling system, to cool the reactor building atmosphere following a reactor coolant system piping rupture, thereby effecting a pressure reduction within the building, and consequently, minimizing the potential leakage of radioactivity from the building to the site and surrounding areas. The spray system also functions to remove radioiodine from the reactor building atmosphere by chemical reaction and to wash suspended particulate radioactivity out of the reactor building atmosphere. The cooling action is accomplished by spraying water into the reactor building atmosphere, in order to remove heat from the steam released by the piping rupture. The fluid for the spray system is supplied from the borated water, sodium hydroxide and-_sodium_thiosulfate_storage tanks and is discharged into the reactor building by a pump in each of the two system circuits. The sodium thicsulfate reacts with radioiodine and removes it from the building atmosphere. In order that the sodium thiosulfate remains stable in the borated water, sodium hydroxide is added to raise the pH of the borated water and maintain it in the alkaline range. The chemical solutions are gravity fed from their respective storage tank's to the line leading to each system pump. The chemical storage tanks and their outlet lines are sized to drain at a rate proportional to the drainage rate of the borated water storage tank.

When the borated water storage tank supply has been exhausted, the reactor building emergency spray system functions in a

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The reactor building emergency spray system has an interface with the dacay heat removal system in that the spray system pumps take suction from the supply headers for the decay heat removal pumps, and during system testing, discharge into the decay heat removal system return line to the borated water storage tank. The system has no normal operating interface with any other plant system with the exception that each pump motor is cooled by water from the nuclear services closed cooling water system.

1.2 <u>Summary Description of System</u> (Refer to B&R Dwg. No. 2034, Rev. 16) The reactor building emergency spray system discharges borated water into the reactor building atmosphere after a loss of coolant accident (LOCA) to cool the steam released due to the casualty and thereby prevent overpressurization by effecting building cooldown. System operation is automatically initiated upon receipt of signals from the safety features actuation system (SFAS). Alkaline sodium thiosulfate and sodium hydroxide are introduced with the spray for radioiodine removal and pH control. The system also functions to provide long term, post-accident building cooling by recirculating the water from the reactor building sump through the spray system.

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The system consists of two circuits each containing a 50% capacity pump for heat removal (100% capacity for iodine removal by sodium thiosulfate injection) which takes suction independently from a decay heat removal system supply header. Each of the two Reactor Building-Spray Pump Suction ... headers is connected to the borated water, sodium thiosulfate and sodium hydroxide storage tanks and to the reactor building sump and can therefore provide the building spray pumps with suction initially from the borated water storage tank and also from the reactor building sump, while at the same time, the decay heat removal system is performing its emergency function. Each of the suction lines to the building spray pumps contains a remotely actuated, electric motor operated stop valve and a check valve in series. The electric motor operated stop valves are normally maintained in the open position and are closed only during normal operation of the decay heat removal system or when isolation of a circuit is required as during maintenance work. The pumps are crossconnected at the suction but are normally isolated from each other by two stop valves in the interconnecting line. Aseparate line fitted with a normally closed, remotely actuated, electric motor-operated-stop valve connects to each pump suction (ine from the sodium thiosulfate storage tank-outlet. These values are automatically opened upon receipt of a signal from the SFAS. The discharge of each pump is routed through an individual reactor building penetration and connects to separate spray headers in the upper portion of the reactor building. Each discharge line is provided with a normally closed, remotely actuated, electric motor operated throttle valve at the pump discharge which opens automatically upon a signal from the SFAS, and a check valve inside the reactor building.

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Provisions have been incorporated into the system to allow testing of the pumps and the spray nozzles. A test connection is provided from each of the pump discharge lines, upstream of the electric motor operated throttle valve, which returns the pump discharge to the borated water storage tank via the decay heat removal system return line to that tank. During in-service testing, the pumps take suction from the borated water storage tank and recirculate back to the tank. Another test connection is provided downstream of each discharge throttle valve to introduce low pressure air or smoke to the spray headers to check for nozzle flow.

The system is automatically activated upon receipt of signals from the safety features actuation system. The electric motor operated valves, necessary for system operation, are opened at a building pressure of 4 psig, and the pumps are started at a building pressure of 30 psig. Remote manual activation by operator action is also provided.

1.3 System Design Requirements

The reactor building emergency spray system is designed to provide sufficient heat removal capability to limit the pressure rise in the reactor building, following a design basis accident, to a point below the 60 psig design pressure of the building, without credit for heat dissipation to the building structure. This capability is predicated upon each of the two 50% capacity circuits delivering 1500 gpm of spray to the reactor building after the accident. However, to provide redundancy, this heat removal requirement is also fulfilled by each of the following: all five of the reactor building emergency cooling system fancooler units in operation; or, three fan-cooler units and one circuit of the building spray system in operation. 196 193

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Therefore, with either the reactor building emergency spray system, the reactor building emergency cooling system or a combination of the two systems being capable of providing adequate cooling of the reactor building atmosphere, the building integrity will be maintained following an accident and the building pressure will be decreased at a rate which satisfies the site criteria.

The water is introduced into the reactor building atmosphere through two spray headers each containing 96 spray nozzles. Each spray nozzle delivers approximately 15.5 gpm upon system actuation immediately following the accident. This flow rate increases slightly with time as the building pressure decreases as a result of cooldown. The water is supplied from the borated water is sodium hydroxide and codium thiosulfate storage tanks until the tanks are empty. Thereafter water collected in the building sump is recirculated through the spray nozzles. The sump water, in all cases, meets the NPSH requirements of the spray pumps with the building spray system in the recirculation mode.

Major system components consist of two pumps, the sodium thiosulfate storage tank, two spray headers with fixed spray nozzles, interconnecting piping and electric motor operated valves capable of automatic opening. The borated water storage tank and the sodium hydroxide storage tank, although not expressly designated as part of the reactor building emergency spray system, serve an integral function with respect to system operation (see Decay Heat Removal System Description, Index No. 20 for further information). The suction line from the borated water storage tank which provides, in part the initial supply of spray water for approximately the first 40 minutes is sized to deliver the expected flows of two decay

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heat removal pumps (3000 gpm each), two high pressure makeup pumps (500 gpm each), and two building spray pumps (1500 gpm each) plus some margin of runout for each pump. The tank will deliver approximately 403,000 gals. of water at a minimum concentration of 2270 ppm boron. The design pressure and temperature of the spray system are 350 psig and 300F, respectively. Major system piping is classified as Nuclear, Symbol N, designed, fabricated, inspected and erected in accordance with ANSI B31.7, Nuclear Piping. The seismic requirements of Class I apply to the entire system including all components.

Monitoring of system performance and control of system operation is provided in the control room.

2.0 DETAILED DESCRIPTION OF SYSTEM

2.1 Components

The components in each circuit are identical and each circuit provides a 50% capacity for building cooling and a 100% capacity for iodine removal. Used in conjunction with the reactor building emergency cooling system, it provides sufficient heat removal to prevent over-pressurization of the reactor building in the event of a loss of coolant accident. Since the system is an engineered safety features system, neither circuit can be out of service except for brief periods during which maintenance is being performed on system components.

2.1.1 Reactor Building Spray Pumps, BS-P-1A/BS-P-1B

The reactor building spray pumps (see Table 1) are single-stage, horizontal-shaft, single suction, centrifugal pumps rated at 1500 gpm each with a total discharge head of 450 ft. The pumps discharge water into the reactor building from the borated water,

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the sodium hydroxide and the sodium thiosulfate storage tanks until the supply in the tanks is nearly exhausted and then recirculate the accumulated water from the reactor building sump back to the reactor building through the spray nozzles. Cooling water for the pumps' motors is supplied by the nuclear services closed cooling water system. The pumps are automatically started by a signal from the safety features actuation system, or can be remotely activated from the control room on the Auxiliary Systems Control Panel Number 3 by operator action. Testing of the pumps' auto-start feature is possible from the Safety Features Actuation Monitoring and Test Panel No. 13. Electric Power supply to the pump's motor is provided from the 4160V engineered safety features busses 2-1E for BS-P-1A and 2-2E for BS-P-1B.

2.1.2 Sodium Thiosulfate Storage Tank BS-T-1

The sodium thiosulfate storage tank (see Table 2) is a vertical cylinder, with a 94" OD and an overall height of 52'-0". The dry capacity of the tank is approximately 17 853 gals. and the tank will deliver 13,000 gals. of 30,000 ppm sodium thiosulfate solution for approximately 40 min. after the LOCA. The sodium thiosulfate solution is discharged into the reactor building with sprayed water and reacts with the iodine to remove it from the building atmosphere. The tank is physically located outside of the auxiliary building. Thermal insulation and redundant electrical neat tracing is provided to maintain the tank temperature above 40F. Heater control is automatic. The tank is designed to withstand an internal pressure equal to a column of

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water 10 ft. above the high liquid level in the tank and a temperature of 150F. A slight nitrogen over-pressure is maintained in the tank to provide an inert atmosphere. The sodium thiosulfate solution is gravity fed to the suction line of each building spray pump through a 4 inch line provided with remotely controlled, electric motor operated valves. The valves open automatically upon receipt of a signal from the safety features actuation system. A relief valve set a 25 psig and a vacuum breaker set at 3 oz/sq.in. are fitted to the tank. A double valved blanked drain and a local sampling connection are provided.

2.1.3

Reactor Building Spray Nozzles

The Reactor Building spray nozzles are manufactured by Spray Co. (model #1713) and are designed to deliver approximately 15.5 gpm at a building pressure of 60 psig with a 40 psi pressure drop through the nozzle. The nozzles are capable of passing particales up to 0.25" in diameter without plugging. Filtering screens in each reactor building sump outlet line are also sized to pass particles up to this dimension. Ninety-six spray nozzles are fixed in each of the two headers. The spray headers follow the contour of the reactor building dome at an elevation of between 449'-09" and 468'-05" within the building.

2.1.4 Borated Water Storage Tank DH-T-1

Although not expressly designated as a component of the reactor building emergency spray system, the borated water storage tank serves an integral function with respect to initial system operation following the loss-of-coolant accident. The tank

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(see Decay Heat Removal System description, Index No. 20, Table 3) is a vertical cylinder, 37'-06" outside diameter, with a vertical straight section of 50 ft. and a self supporting domed roof. The overall height of the tank is 60'/04-3/4" and the dry volume if 472,964 gals. The tank is physically located outside of the auxiliary building. Thermal insulation and redundant electrical heat tracing is provided to automatically maintain the liquid at a minimum temperature of 40F. The tank will deliver approximately 403,006 galr. (Normal level to Lo/Lo Level) of water at a minimum concentration of 2270 ppm boron and provides a source of borated water for the building spray pumps, as well as the decay heat removal pumps (for low pressure injection) and the high pressure makeup pumps, for approximately 40 minutes after a LOCA.

2.1.5. Sodium Hydroxide Storage Tank DH-T-2

The sodium hydroxide storage tank is also not expressly designated as a component of this system but serves an integral function following a LOCA. The tank (see Decay Heat Removal System description, Index No. 20 Table 4) is a vertical cylinder, 84" in outside diameter with an overall height of 52 ft. and a dry volume of approximately 14,285 gal. of water at a concentration of 20,000 ppm NaOH. The delivered volume following the LOCA is approximately 11,600 gals. The sodium hydroxide establishes an alkaline pH in the borated water which is injected into the reactor building after the accident to maintain the stability of the sodium thiosulfate which is added for iodimeremoval. The tank is physically located outside of the auxiliary building and thermal insulation is provided. Redundant electrical

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heat tracing is installed around the tank to automatically maintain the liquid temperature at approximately 40F. A slight nitrogen overpressure is maintained in the tank to provide an inert atmosphere.

2.1.6 Major System Valves

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Reactor Building Spray Pump Discharge Valves-BS-VIA, BS-VIB One 350 psig, 300F, 8 inch, SS, electric motor operated globe valve is provided in the discharge line from each reactor building spray pump. The valves are opened automatically within 10 secs. by a signal from the safety features actuation system. Remote manual operation of each valve is provided from the coolant Systems Monitoring Panel No. 8 in the control room. Cycling of the valves for periodic test purposes is controlled from the Safety Features Actuation Monitoring and Test Panel No. 13. During system operation, as the reactor building pressure decreases, the valves are remote manually throttled to prevent pump runout. Power supply to the electric motor valve operators is provided from the 480V motor control centers 2-11EA for BS-VIA and 2-21EA for BS-VIB.

Reactor Building Spray Pump Suction Valve from Decay Heat Removal Suction Headers - BS-V3A, BS-V3B

One 200 psig, 300F, 10 inch, SS, electric motor operated gate value is provided in the suction line from the decay heat removal system suction headers to each building spray pump. These values are normally maintained in the open position except during operation of the decay heat removal system when the removal system is serving its normal functions. In these cases, BS-V3A and BS-V3B must be closed by operator action to isolate the

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building spray system. The valves are remotely controlled from the control room by switches located on the Auxiliary Systems Control Panel Number 3. Power to the electric motor valve operators is supplied from the 480V motor control centers 2-11EA for BS-V3A and 2-21EA for BS-V3B.

Sodium Thiosulfate Storage-Tank to Reactor Building Spray Pump Suction Lines, BS-V4A and BS-V4B

One 350 psig, 300F, 4 inch, SS, electric motor operated gate valve is provided in the gravity feed line to each building spray pump suction line from the sodium thiosulfate storage tank. The valves are opened automatically within 20 seconds by a signal from the safety features actuation system, to admit the sodium thiosulfate to the pumps for discharge into the building atmosphere. Remote manual operation of each valve is also provided from the control room on Coolant Systems Monitoring Panel Number 8. Cycling of the valves for periodic test purposes is controlled from the Safety Features Actuation Monitoring and Test Panel No. 13. Power to the electric motor valve operators is provided from the 480V motor control centers 2-11EA for BS-V4A and 2-21EA for BS-V4B.

2.2 Instruments, Controls, Alarms and Protective Devices

Instrumentation is provided in the control room on the ... Auxiliary Systems Control Panel Number 3 for the reactor building emergency spray system to monitor system performance during testing, standby and during actual operation. (See Table 3). A listing of panel mounted annunciator, relief valve and vacuum

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breaker setpoints is given in Table 4. Alarm conditions are annunciated in the control room on the Coolant Systems Monitoring Panel No. 8.

The reactor building spray flow in each circuit is monitored and indicated in the control room. High and low flow alarm contacts are provided for annunciation. The low flow alarm is interlocked with the reactor building high-high pressure monitors to annunciate only during an emergency condition, i.e., when the building high-high pressure monitor has been tripped. This arrangement permits the Low-Flow Alarm to function as a monitor to verify that the Building Spray pumps--have started. Local instrumentation is also provided to indicate the suction and discharge pressure of each pump with low suction pressure alarmed in the control rocm.

The temperature and level in the sodium thiosulfate storage tank is monitored and indicated in the control room with high and low condition for each parameter, annunciated. A gauge glass is fitted to the tank for local level indication. The temperature of the solution in the tank is automatically maintained by redundant electrical heat tracing. A tabulation of the instrumentation to the borated water and sodium hydroxide storage tanks can be found in the Decay Heat Removal System Description, Index No. 20.

A relief value set at 350 psig is provided at the suction of each building spray pump to preclude overpressurization from inadvertent reactor coolant system leakage through closed values when the spray system is idle during normal reactor power operations. A vacuum breaker and pressure relief value are fitted on the sodium thiosulfate storage tank to prevent damage to the tank.

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For details concerning actuation of the reactor building emergency spray system, refer to the Safety Features Actuation System description, Index No. 50.

3.0 PRINCIPAL MODES OF OPERATION

3.1 Startup

Startup of the reactor building emergency spray system consists of testing the operation and performance of the system and preparing it for normal stand-by service. The borated water storage tank is filled with demineralized water and boric acid to establish a 2270 ppm minimum boron concentration if this has not already been accomplished. With the circuit electric motor operated discharge valve closed and suction lined up from the borated water storage tank, each pump is started individually and flow is recirculated to the storage tank. Flow rates and pump suction and discharge pressures are noted and recorded for future reference in determining system performance. System piping up to the circuits' discharge valve BS-VIA/BS-VIB are maintained filled with borated water. The automatic actuation feature of all related equipment, including all electric motor operated valves must also be tested to ensure proper operation. An air or smoke supply is introduced into the nozzle air test connection for each circuit to check for free flow through the nozzles. Visual observation of the ribbon indicators attached to each nozzle or of the smoke is required to verify proper nozzle operation.

The sodium thiosulfate storage tank is filled with demineralized water and sodium thiosulfate to produce a 30,000 ppm concentration in the tank. The tank outlet line and each branch to the building spray pump suction line, up to the motor operated valve is filled.

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and vented. A nitrogen-overpressure at approximately 2-psig-is introduced into the tank to maintain an inert atmosphere. The system is then lined-up-and maintained in a standby condition, ready for emergency operation. It must be ensured that the sodium hydroxide storage tank is also filled and at the prescribed concentration of 20,000 ppm NaOH.

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A low point drain line is provided in each circuit inside the reactor building and fitted with manual stop valves BS-V106A/ BS-V106B. The purpose of the drain lines is to prevent water from reaching the spray headers by leakage through the building spray pumps' discharge valve during system testing. These drain lines are sized to pass approximately 16 gpm (flow through one spray nozzle) and must be opened prior to reactor startup and remain open during reactor operation.

3.2 Normal Operation

The reactor building emergency spray system serves no function during normal plant power operation. The system provides an engineered safety features function and is actuated by signals from the safety features actuation system following a reactor coolant system piping casualty which increases the reactor building pressure above pre-set points. The system can also be manually placed in service by operator action, if required.

Upon receipt of an actuation signal, the circuits' discharge valve BS-VIA/BS-VIB, the sodium thiosulfate supply Valves, BS-V4A/BS-V4B, and the valves in the lines from the borated water storage tank (DH-V5A/DH-V5B) and sodium hydroxide storage tank (DH-V8A/ DH-V8B) are automatically opened followed by automatic starting

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of the spray pump, BS-P-1A and BS-P-1B. The pumps take suction independently through 10 in. lines, fitted with electric motor operated valves BS-V3A/BS-V3B (normally open), from each decayheat removal pump suction header. The suction headers are supplied with water from the borated water and sodium hydroxide storage tanks through independent lines fitted with safety features actuated, electric motor operated valves DH-V5A/DH-V5B and DE-V8A/DH-V8B. The suction lines to the pumps can be crossconnected but are normally maintained isolated by manual stop valves, BS-V101A and BS-V101B. A 4 in branch line from the common-outlet-of-the-sodium-thiosulfate-storage tank connects to-the-suction-line-of-each-building-spray_pump_ Each-branch line-is-provided with-a-safety-features-actuated_electric-motoroperated_valve,-BS-V4A/BS-V4B- The pumps discharge to independent 8 in. lines fitted with electric motor operated throttle valve BS-VIA/BS-VIB. These valves are opened fully upon a SFAS Signal but are ... remote : manually throttled in order to prevent pump runout as the reactor building pressure decreases due to cooling of the atmosphere after the accident. Downstream of the throttle valve, each pump discharge line enters the reactor building through a separate penetration, R-586 for circuit A, and R-583 for circuit B. Downstream of the building penetration, the piping size is reduced to 6 in. and each line is provided with a check valve for building isolation. Each circuit is then routed to one of the two spray headers in the upper part of the reactor building. Physical space limitations within the building required that the 6 in. supply line to each spray header be reduced into 4-4in. risers, ascending along the reactor building wall and reconnecting at the header.

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Before the supply of water in the borated water storage tank is exhausted, (approximately 40 min.), the control room operator is alerted by annunciation of the low-low storage tank level alarm. At this time, the suction supply to the pumps must be ____ transferred from the storage tank to the reactor building sump. The operation is performed by action of the control room operator. The electric motor operated valves, DH-V6A/DH-V6B, in each of the reactor building sump lines to the decay heat removal pump suction headers are opend, and the supply valves DH-V5A/DH-V5B from the borated water storage tank, BS-V4A/BS-V4B from the sodium thiosulfate storage tank and DH-V8A/DH-V8B from the sodium hydroxide storage tank.to the headers are closed. Hand switches on the Safety Features Actuation Monitoring and Test Panel No. 3 provide for negating the safety features actuation signal (once the signal has been tripped) so that these valves may be closed. Once the safety features actuation signal has been negated, these valves are closed by depressing their respective actuation switches from the control room. The reactor building emergency spray system, in this mode, recirculates the water from the reactor building sump through the spray system, and discharges the water into the reactor building atmosphere to continue iodine removal as well as building cooldown and depressurization.

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3.3 SHutdown

When the building spray system is shutdown, as is the case during normal reactor power or shutdown conditions, it is maintained in a standby status with all valving except the safety features actuated, electric motor operated valves positioned for system operation, and the pumps available for automatic start. If

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maintenance to equipment in one circuit of the system is required, it must be ensured that the other circuit is fully operable and available in the event of an emergency. To shutdown a circuit for maintenance, it is only necessary to de-energize the pump and the safety features actuated valves, close and de-energize the electric motor operated pump suction valve (either BS-V3A or BS-V3B), and close the associated manual valves to isolate the circuit and/or component requiring maintenance.

Following a system test, the building spray pump(s) must be manually stopped and the valves, opened for the test, must be closed and the system control switch positioned for automatic operation.

3.4 Special or Infrequent Operation

Provisions have been incorporated into the system to allow testing of each circuit pump and for testing spray nozzle flow during reactor operation. Pump performance can be determined by operating the pump taking suction from the borated water storage tank through electric motor operated valve DH-V5A or DH-V5B and discharging through manual test valve BS-V103A or BS-V103B and BS-V104 back to the storage tank via the decay heat removal system test line. The suction and discharge pressures of the pump and the circuit flow is noted and recorded for comparison with initial and prior test results to determine system performance.

The nozzle flow test is performed by introducing air or smoke through the nozzle test connection, for each circuit, fitted

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with manual stop valve BS-V130A or BS-V130B. The air flows through the circuit piping to the spray header in the reactor building and free flow is confirmed by visual observation of the smoke or the ribbon indicators affixed to each nozzle.

Sampling of the water contained within the sodium thiosulfate storage tanks is periodically performed to ensure an adequate concentration of the required chemicals and to determine water quality. Sample taps are fitted to each tank for this purpose.

3.5 Emergency Operation

Reactor building emergency spray is initiated upon an abnormally high reactor building pressure sensed by redundant pressure monitors within the building. System activation is a function of the safety features actuation system (see System Description, Index Number 50).

Operation of the system in the emergency mode is identical to that which has been described under "Normal Operation", Section 3.2 of this system description.

Additional sodium hydroxide and sodium thiosulfate may be added to the recirculating water during post-accident operation, if deemed necessary. The solution is added to the respective storage tank from the caustic mixing tank, via the addition pump, in the chemical addition system and then introduced into the recirculating water by opening the appropriate storage tank outlet valve (s), once a water level in the storage tank has been established.

HAZARDS AND PRECAUTIONS

The principal hazard associated with this system is inadvertent actuation when no emergency condition exists. Such an occurrence with the reactor in operation or in a shutdown condition could cause damage to equipment and electrical wiring within the reactor building. Since manual activation of the system is possible from the safety features actuation panel, extreme care must be exercised to prevent this occurrence. Also, prior to routine periodic test of the system pumps, a visual observation of the electric motor operated throttle valves BS-VIA and BS-VIB should be made to ensure that the valves are fully closed. <u>Pump Details</u> Identification Number Installed Manufacturer

Model No.

Type

Rated Sp.ed, rpm Rated Capacity, gpm (U.S.) Rated Total Dynamic Head, ft. Submergency required at rated flow, ft. Design Pressure, casing,psig Design Temperature, ^OF Lubricant/Coolant Min. Flow Requirements, gpm

TABLE 1 .

REACTOR BUILDING SPRAY PUMP

2 1

Motor Details

Manufacturer Type Enclosure Rated Horsepower Speed, rpm Lubricant/Coolant Power requirements BS-P-1A, BS-P-1B Two Babcock & Wilcox, Ltd., Canada SMK 6 x 8 x 13 Single Stage, Horizontal Shaft, Single Suction, Centrifugal 3600 1500. 450 14 350 300 Oil/Water None

Westinghouse Electric Corp. LLD Horizontal Totally enclosed 250 3600 Oil/Water 4160V, Amps (Full Load) 60 Hz, 3-Ø

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TABLE 1 (Continued)

Power Source (for each pump motor).

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BS-P-1A:-4160V. Engineered Safety Features Bus 2-1E BS-P-1B:-4160V. Engineered Safety Features Bus 2-2E

Classification

Code

Quality Control

Seisimic

Cleanliness

Level N-2 2 I C

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Sodium Thisolpha	ate Storage TANK
Identification	BS-T-1
Manufacturer	Buffalo Tank Div.
Capacity-gallons	17,853
Installation	Vertical
Outside diameter and length	94" O.D. x 52' High
Skill Material	304 S.S
Shell Thickness	9/16"-3/16"
Design temperature, ^O F	150 [·]
Design pressure,	High Liquid Level Plus 10 ft. Water
Corrosion allowance, in.	None
Design Code	ASME-1968 Sec. VIII Div. 1
Code stamp required	NO
Minimum Temperature F.	40
Electric heating/Source	Redundant Heat tracing
Classification	<u>Level</u>
Code	N-3
Quality Control	3
Seismic	I
Cleanliness	C

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NURME AND ROE, INC.

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		INTEL	EDITATION AND CONTROLS					
DUTERTION	DESCRIPTION	NACTION	LOCATION	NI	INNUT RANCE	OUTPUT AANGE	SETHOINT *	
-1-11	Differential Presents	Indicates. flow from M-P-13 her	AI-9-94' Jo'eguades Id	Orifice	0-1800 GM	0-300. NO	\$	-
-1-10	Differential Pressure	Indicates flow from M-P-18 Pap	Discharge of 86-P-18	Orifice	0-1800 GM	0-300° N,0	\$	
-1-011	Differential Presents	Transit Diff. Press. signal.	Discharge of M-P-1A	۰.	0-300* M30	± 10 VD.C.	\$	
-1-0-1-	Differential Pressure	Transait Diff. Press. signal.	Discharge of 85-P-18	۵.	0-300° M_0	± 1040.C.	**	
	Indicator	Indicates flow from M-P-IA	Passel No. 3	Yant. Gauge	10 4 80	0-1000 GMM	•	
-1-res	Indicator	Indiantes flow from 88-P-18	Passi No. 3	Vart. Gauge	10 4 85	0-1800 GPM	4	
-1-m1	rior Alas	Ki-tor flow Alars M-P-IA	; 1	HI-LO BUILD	± 10 V CC	0-1600 GM	N1-1700 GPM	
	. The Alars	Ni-Low flow Alarm M-P-LB		ul-to Mitch	2 10 V CC	0-1000 GM	N1-1700 GMI	
1-14-1-	Press. Indicator	Indicates Disch. Press. M-P-1A	TOOM	TAID	0-400 MIG	\$	e a	
-3-713	Press. Indicator	Indicates Disch. Press Mi-P-18	TICOT	DIAL	0-400 MIG	**	N / N	
	Level Trumsities	Trumit Level of fash M-1-1	Storege Tank NI-T-1	• •	0-50 R.	± 10 V BC	ş	
	Lavel Indicator	Indicate Lavel of Tank M-T-1		Bailoy Type MT	± 10 V 00	0-50 FT.	\$	
3-1-	Level Alars	Ni-to Bignal for Tank M6-7-1	1	Ki-Lo Mitch	± 10 V KC from 84-3-Let	\$	11-44.5°, 16-42.5°	
	Freeses Gugs	Indiants corer que press. co MI-7-1	1 8	Bourdon	0-1 MIG	\$	\$	
F.	Treporture Ilant	Renes and indicate tamp of MS-T-1	14	Plat. #10	6-100 ⁰ F	100 of-	4	
÷.	Top. Translate	Convert Maelat. eiga. to voltaga DC		B.C. Convert.	0-100°r	± 10 V 00	5	-
1-1-	two. Indiator	Two. Audout of M-T-1	1	Mailay-NY	± 10 V GC	0-300°r	5	
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			TALE 3 (Continued)	•			
pomnonio	and more	Lancia de la constante	IOCATION	퇸	ENN THN	OUTPUT MAKE	JETROINE
18-1-8	Tw. mist	Bistable Content for Two. Cont. (Me-7-1)	:1	Ki-Lo signal mailes	+ 10 V IC from	\$	- 110 -
-1-13	1	Mistable Contact for Twop. Alarne (18-7-1)	1	Ki-Lo Signal Monitor	+ V CC from	\$	10-30 F.
		land mitch Control for M-VM	1	Putch : Polition Lynt.	§.	\$	\$
		had hitch Control for M-VIB	1	Buitch e Peeltion Ligt.	\$	\$	\$
MS-FT6-1400	Flow Mund Actuated Builtin	Actuates Ba-Via fodim Thiosulphate Into Beactor Building Spray	. 12	Puebbuttom	\$	\$	\$
M0-718-1401 (M0-V40)	Plan Intel Arturted Builds	Actuates 25-V48 Sodium Thiosulphate into Associat Building Spray	1	Puebbut ton	\$	\$	\$
1011-17-M	· Lami Indianter	Indicates lavel of 26-7-1 Bodium Thiosulphate Storege Turk	1.	pitt. maa.		-95-0	\$
. 1001-140-M	bitt. Ressure Indicator	" Indicate DP across M-42 to suction of M-P-18	Lise at Valves B4-V1208 & B4-V1218		0-100" Matar	0-135" Mater	\$
NON1-M-M	Nue. Mich	Actuates NJ-NL-1404 low suction press. to NJ-P-18	Auction line to 85-P-18 at valve 85-V1328	Dispirage	0.25-16 MIG	ş	912 53
(10-54 sectors)	diff. Resoure indicator	Indicates DP-across M6-U1	Line at Valves BS-VI30A - BS-VI31A	10	0-100" Matar	0-135" Water	\$
N0+1N-FR	1	Actuates N-ML-100	Suction line to NJ-P-1A at Valves NS-V122A	Diaphrage.	DIM 91-66'0	\$	
(81-P18-1407	Flow Mand socurted witch	Actuates Valve B5-V1B flow to Beaut. Bidy. Spray Mossies."	i)	Pueblut ton	ş	5	Ş
M-RL-1407	Position Lights	Indicates Open-Cióse on M6-V-18	Paral 15	B-30-8,0	\$	**	\$
141-1-1408	. These thead actuated switch	Actuates Valves 25-VIA flow to React. Blóg. Sprey Notales.	į	Puebbut ton	\$	5	ş

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BUTION	CONTINUES.	PACTION	ICONTON	뙲	JANT AMG	PUTWT MAGE	JETPOINT
	Presence Miltoh	betwates from Nigh Presence in Peaclor Bidg. (Green Channel) Bd-Vih, B	5) 1	1	0-10 MIG	ş	• 1010
1921-8-	Trauer Mich	Actuates from Nigh Pressure in Desotor Bidg. [Tellow Chennel] BS-Vik, B		1	0-10 MIG	ş	•
of 61-84-	Trauma Mith	Actuates from Nigh Freesure In Reactor Nidg. (Red Channel) NM	8	Miles	0-10 MIG	\$	•
1111-11-	Tranur Mitch	Actuates from Migh Pressure in Desotor Midy. (Green Channel) A.P.S.			0-10 MIG	\$	• 110
tin-m-	Pressure build	Actuates from Nigh Pressure in React. Bidy. (Tellow Chennel) R.P.S.		1	0-10 MIG	\$	• 816
tist-w-	Freenure Pultab	Actuated from Nigh Pressure in Neast, Bidy, (Biue Channel) R.P.G.	55 14	-	0-10 MIG	\$	• 111
-114-3353	Bouting Value	Press. Test for M-M-1151	Reck 473	Solenoid	0-100 MIG	\$	
-114-3354	Acuting Valve	Press. Test for 88-M-1259	Rick 455	solenoid	0-100 MIG	**	4.4
	Mouting Valve	Press. Test for 24-79-1255	Tech 467	Solenaid	0-100 MIG	\$	\$
	Mouting Valve	Press. Test for 26-P6-1256	Reak 472	Bolenoid	0-100 MIG	**	\$
	Noutled Value	Press. Test for 26-PS-1257	Ruck 455	Solenoid	0-100 1410	**	\$
-rrd-3254	Routing Valve	Press. Test for MI-18-1258	Rath 467	Solenoid	0-100 Mild	**	*
-174-3358	Acuting Valve	Press. Test for MS-PG-1259	Rack 472	Bolenoid	0-100 1010	**	\$
	Mouting Valve	Press. Test for M-M-3260	Reck 455	Bolenoid	0-100 1310	***	**
-1412-1741	Mouting Value	Press. Test for MS-PS-1261	Rack 467	solenoid	0-100 MIG	M/A	K *
-PTV-3270	Routing Valve	Press. Tast for \$5-16-1570	Rach 472	Solenoid	0-100 MIG	**	¢.
	Routing Valve	Press. Test for M-MS-1571	Ruck 455	Solendia	0-100 MIG	\$	\$
1	Routing Value	Frees. Test for 14-19-1572	Mcd. 6671	belenzia	0-100 MIG	WAI	\$
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ELSE-414-98	Acuting Valve	Frass. Test for M-rs-1573	Mack 452	Bolensid	0-100 MIG	*	\$
M-41-3439	Position Lights	Indicate Open-Close an M9-V146	Pernel 15	1mg 01-8	\$	\$	*
010-EL-3840	Preities Lights	Indicate Open-Close on M-VI47	Passel 15	1mg 0(-8	\$	**	-
. 1961-73-M	Preities Lights	Indicate Open-Class on M8-Vies	Parmel 15	1-30 Dual		*/*	\$
M-41-3013	Preitice Lights	Indicat Open-Close on Me-v169	Panel 15	1mg 0(-8	5	***	*
	Pressure Builds	Actuated from High Pressure in React. Bidy. (Red Channel)	8	1		\$	
1945-MA-3841	Mouting Valme	Press. Test Cor No-W-1941	Reak 472	Belenoid	0-100 MIG		
	Pressure Builds	Actuated from Nigh Pressure in Readt. Bidg. (Green Channel)	Mat 155	na lion	0-10 MIG	\$	
0066-AL4-94	Routing Valve	Frees. Test for 10-1998	Reok 455	Solenoi.	0-100 MIG		*
886C-M-M	Pressure Builds	Actuated from High Presence in Beact. Bidg. (Fellow Chennel)		1	0-10 MIG	\$	
88-PTV-3983	ADMLING VAIVA	Press. Test for M-N-1989	Rech 467	Boleaold	0-100 MIG		\$
N-M-134	1	Records press. in React. Bldg.	1	Mint Recorder	10-50 M DC 10-50 M .00	-9-10 MIG 0-100 MIG	\$
1-9000-44-98	Press. Transmitter	tranamits press. in Meaot. Bidg.	Rach 455	Bellows	-3-10 MIG	10-50 M DC	\$
5-00()-M-M	True Mitch	Actuated from High Presence in Readt. Hidy. (Alarn)	Cable Noom	solid state	10-50 M CC	\$	2
E-880-11-18	Press. Trasmittar	Transmits press. in Masot. Bldg.	Real 455	Millon	0-100 MIG	10-50 M DC	\$

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MA-ML-1404	28 Bautor Mililian Sprey Namp Buction Press. 10.	•		N-M-1404
M-ML-1406	24 Assotat Building Speay hung suction Press. Is.	1	6.5 mia	90+1-W-84
88-MH-1413	Passtor Building Prass. BL.	30 MIG	1	1-111-54-5M
BE-63-3039	Me-V146 Most Open	1	1	(1-18) 891A-88
M-43-3840	Me-V147 Mat Open	1	1	12-147 (81-7)
1101-11-04	. Ma-V148 Not Open	1	1	(L-78) 801A-98
10-17-1943	Me-Vids Not Open	1	1	(L-78) 611A-58
M-44-1615	MA Spear hang Buction Mandar Valva slosed.	1	•	130-01
N-1-104	24 Assetor Building Speer Parp . Flow Hi/La	84	815	1-2-1-2
101-U-W	28 Assotat Building Spray Name	840	8 E	
80-17-FR	bod. Micaultate Storage Task Lavel Mi/Lo		we	7-12
801-18-18	ted. Thiosulfate Storage Test Teap. Mi/lo		* *	
N-134	Meastar Building Spray Nump Overload	1	1	74/14-1-14
M-137-137	Reactor Bidg. Sproy Part Trip	1	•	307/38-P-14 6

Coolant Systems Monituring Passel No. 8-81 .. 114-61 Coolant System Monitoning Paral No. 8-41 Coolant Systems Monitoring Musi No. 8-81 Coolant Systems Monitoring Panel No. 8-82 6. 13-45 Coolant Systems Monitoring Muel No. 8-Dl Coolast Systems Wonitoring Panel 3 Coolant Systems Monitoring Panal ingineered Safety Peatures Pul. ingineered Safety Peatures Pul. ingineered Safety Peatures Pol. inginaaced Safety Features Pal. 0-1800 GM MD 0001-0 0-100 MIG -90. 1

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ORS AND PROTUCTIVE DEVICES SET POINTS

TABLE 4

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Coolant Systems Monitoring Paral No. 8-43 Coolant Systems Munitoring Pasel No. 8-71

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TABLE 5

COMPUTER LIST (DIGITAL)

INPUT NO.		DESCRIPTION	INSTRUMENT V. TAG NO.	INPUT CONDITION FOR OUTPUT STATUS CHANGE	t j	USES
2824		ES ACT A BLDG ISLN MNL TEST GP1	1x1E/RBA	MANUAL TEST	Å A	LARM ,
2825		ES ACT A BLDG ISLN MNL TEST GP2	1x2C/RBA	MANUAL TEST	. A	LARM "
2826		ES ACT A BLDG ISLN MNL TEST GP3	1x3e/RBA	MANUAL TEST	A	LARM
2827		ES ACT A 2/3 LOGIC BLDG ISLN GP1	63Z1E/RBLA, RB2A, RB3A	4 PSIG	7	LARM
2828		ES ACT A 2/3 LOGIC BLDG. ISLN GP2	63Z2C/RB1A, RB2A, RB3A	4 PSIG	,	LARM
2829		ES ACT A 2/3 LOGIC BLDG ISLN GP3	63Z3E/RBLA, RB2A, RB3A	4 PSIG	. ,	LARM
2830		ES ACT A BLDG ISLN CH1 DEFEATED	43X/RBLA & 43Y/RBLA	4 PSIG .	,	ALARM
2831		ES ACT A BLDG ISLN CH2 DEFEATED	43X/RB2A & 43Y/RB2A	4 PSIG	,	ALARM
2832		ES ACT A BLDG ISLN CH3 DEFEATED	43X/RB3A & 43Y/RB3A	4 PSIG	,	ALARM
2833		ES BLDG ISLN SW ACT A CH1 TRIP	63X2/RBLA	4 PSIG	A	LARM
2834		ES BLDG ISLN SW ACT A CH2 TRIP	63X2/RB2A	4 PSIG	,	ALARM
2835		ES BLDG ISLN SW ACT A CH3 TRIF	63X2/RB3A	4 PSIG	1	ALARM
2836	-	ES BLDG SPRAY SW ACT A CHI TRIP	63X/RB4A	30 PSIG	A	LARM
2837	96	ES BLDG SPRAY SW ACT A CH2 TRIP	63X/RB5A	30 PSIG	A	LARM
2838	218	ES BLDG SPRAY SW ACT A CH3 TRIP	· 63X/RB6A	30 PSIG	1'	ALARM .

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TABLE 5 (Continued)

COMPUTER LIST (DIGITAL)

INPUT NO.	DESCRIPTION	INSTRUMENT TAG NO.	INPUT CONDITION FOR OUTPUT STATUS CHANGE	US ES
2839	ES BLDG 2/3 LOGIC RB SPRAY	63X/RB4A, RB5A, RB6A	30 PSIG	ALARM
2849	ES ACT B BLDG ISLN MNL TEST GP1	1x1E/RBB	MANUAL TEST	ALARM
2850	ES ACT B BLDG ISLN MNL TEST GP2	1x2C/RBB	MANUAL TEST	ALARM
2851	ES ACT B BLDG ISLN MNL TEST GP3	1x3e/RBB	MANUAL TEST	ALARM
2852	ES ACT B 2/3 LOGIC BLDG ISLN GP1	63Z1E/RB1B, RB2B, RB3B	4 PSIG	ALARM
2853	ES ACT B 2/3 LOGIC BLDG ISLN GP2	63Z2C/RB1B, RB2B, RB3B	4 PSIG	ALARM
2854	ES ACT B 2/3 LOGIC BLDG ISLN GP3	63Z3E/RB1B, RB2B, RB3B	4 PSIG	ALARM
3047	ES ACT B BLDG ISLN CH1 DEFEATED	43X, 43Y/ RBlb	4 PSIG	ALARM
3048	ES ACT B BLDG ISLN CH2 DEFEATED	43X, 43Y/ RB2B	4 PSIG	ALARM
3049	ES ACT B BLDG ISLN CH3 DEFEATED	43X,43Y/ RB3B	4 PSIG	ALARM
3278	ES BLDG ISLN SW ACT B CH1 TRIP	63X2/RB1B	4 PSIG	ALARM
3279	ES BLDG ISLN SW ACT B CH2 TRIP	63X2/RB2B	4 PSIG	ALARM
3280	ES BLDG ISLN SW ACT B CH3 TRIP	63X2/RB3B	4 PSIG	ALARM
3281	$\frac{9}{5}$ es bldg spray SW act b chl trip	63X/RB4B	30 PSIG	ALARM

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TABLE 5	(Continued)	
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COMPUTER LIST (DIGITAL)

INPUT NO.	DESCRIPTION	INSTRUMENT TAG NO.	INPUT CONDITION FOR OUTPUT STATUS CHANGE	USES
3264 :	ES BLDG SPRAY SW ACT B CH2 TRIP	63X/RB5B	30 PSIG	ALARM
3265	ES BLDG SPRAY SW ACT B CH3 TRIP	63X/RB6B	30 PSIG	ALARM
3050	ES BLDG 2/3 LOGIC RB SPRAY	63X/RB4B, RB5B, RB6B	30 PSIG	ALARM
3167	4 PSI RB PRESS RED CH TRIP	BS-PS-3570	CH TRIP	ALARM SEQ. MON.
3168	4 PSI RB PRESS GRN CH TRIP	BS-PS-3571	CH TRIP	ALARM SEQ. MON.
3169	4 PSI RB PRESS YEL CH TRIP	BS-PS-3572	CH TRIP	ALARM SEQ. MON.
3170	4 PSI RB PRESS BLUE CH TRIP ,	BS-PS-3573	CH TRIP	ALARM SEQ. MON.

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	TABL COMPUTER L	E 5 (Continued) IST (ANALOG)		•	
INPUT NO.	DESCRIPTION	INSTRUMENT TAG NO.	ALARM	LIMINS	USES .
0097 1668 1 1669	RB WIDE RANGE PRESS. BLDG SPRAY PMP A MOT STATOR BLDG SPRAY PUMP B MOT STATOR	BS-PS-1412-2 BSP-52-TE6 BSP-52-TE12		30 PSIG 266F. 266F	ALARM ALARM

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METROPOLITAN EDISON COMPANY.

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Wilda R. Mullinix, NRC